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REDUCED MAGNETIC NOISE AND CURRENT RIPPLE AUTOMOTIVE ALTERNATOR

[0001] The present invention relates generally to rotating electrical machines, and more particularly, to a stator structure configured to generate a reduced amount of audible noise.

Technical Field

[0002] Alternators are rotating electrical machines used in vehicles for generating electric power to charge the battery when the rotor of the alternator is turning at a sufficient speed. Those skilled in the art will recognize that alternators are also referred to as generators. In the design of automotive vehicles, manufacturers are continually trying to reduce the audible noise generated from various components in the vehicle. Alternators generate audible noise due to the magnetic forces in the alternator and other factors, such as fan noise.

[0003] Current ripple in the output is also undesirable. Current ripple occurs when the AC output of the alternator is rectified. The rectification is a summation of the output currents from the various phases of the machine. The DC current therefore has some fluctuation. Three phase alternators are common. In a three phase alternator, six crests and valleys occur over one electrical cycle which is defined as the rotor rotation through one pair of magnetic poles. Current ripple has also been found to contribute to audible noise. When the current at the output has ripple,

the input torque also ripples. The input torque ripples in response to maintaining a relatively constant speed in the rotating machine. This phenomenon causes audible noise as well.

[0004] Therefore, it would be desirable to provide an alternator stator configuration that reduces current ripple and thus, audible noise.

Summary of the Invention

[0005] The reduced oscillation of magnetic flux of the present invention provides an alternator with reduced noise and smoother output.

[0006] In one aspect of the invention, an electrical machine includes a stator core having slots and a set of windings disposed within the slots. The windings are configured in 2N+1 phases, where N is an integer greater than 1. Such a machine is particularly useful for automotive alternators.

[0007] One advantage of the invention is that because a smoother output signal is produced, lower electromagnetic interference is generated.

[0008] Other advantages and features of the present invention will become apparent when viewed in light of the detailed description of the preferred embodiment when taken in conjunction with the attached drawings and appended claims.

Brief Description Of The Drawings

[0009] Figure 1 is a cross-sectional view of an electrical machine incorporating the present invention.

[0010] Figure 2 is a partial cut-away perspective view of a stator core according to a seven phase (N=3) implementation of the present invention.

[0011] Figure 3 is a plan view of a stator core according to the present invention.

[0012] Figure 4 is a schematic view of a first embodiment of a winding circuit according to the present invention.

[0013] Figure 5 is a schematic view of a second embodiment of a winding circuit according to the present invention.

[0014] Figure 6 is a current versus time plot of a three phase alternator of the prior art.

[0015] Figure 7 is a current versus time plot of a seven phase (N=3) alternator according to the present invention.

[0016] Figure 8 is a plot of noise versus speed of a winding according to the present invention compared to existing windings.

Detailed Description Of The Preferred Embodiment

figures, [0017] In the following the same reference numerals will be used to identity the same components in the various views. Although one embodiment of an alternator is illustrated, the stator winding circuit embodiments described below may be used in a variety of types of electrical rotating machines including liquid-cooled alternators, air-cooled alternators and various including multiple configurations of alternators rotor alternators and the like.

[0018] Referring now to Figure 1, an alternator 20 includes a front housing portion 22 and a rear housing portion 24 which are suitably bolted or otherwise attached together. Front housing portion 22 and rear housing portion 24 are preferably metallic. The housing portions 22 and 24 may be configured with openings for air cooling or fluid passages for liquid cooling as is known to those skilled in the art. A rotor 26 is included within front housing portion 22 and rear housing portion 24. Those skilled in the art will recognize rotor 26 as being generally of the "claw-pole" variety. A plurality of permanent magnets 28 may be disposed within rotor 26 in order to enhance the electrical output of alternator 20.

[0019] Rotor 26 includes a shaft 29 having two slip rings 30 and 32 which are means for providing electrical power from a voltage regulator (not shown in the particular sectioning employed in Figure 3) to a field coil 34 disposed within rotor 26. Also coupled to shaft 29 is a pulley 36, or other means for rotating rotor 26. Shaft 29 is rotatably supported by a front bearing 50, itself supported by front

housing portion 22, and a rear bearing 52, supported by rear housing portion 24.

[0020] A stator 54 is disposed in opposition to rotor 26. Stator 54 includes a ferromagnetic stator core 56, on which stator windings 58 are wound.

A rectifier 70, coupled to stator windings 58 in order to rectify the alternating current output generated in stator windings 58 by the operation of alternator 20, mounted to rear housing 24. Rectifier 70 is formed of many rectifying elements which are preferably diodes. other rectifying elements such as transistors may also be Rectifier 70 includes a negative rectifier plate 72, which forms the common connection for the cathodes of the "negative" diodes 72A. Rectifier 70 also includes positive rectifier plate 74, which forms the common connection for the anodes of the "positive" diodes 74A. Negative rectifier plate 72 and positive rectifier plate 74 are electrically insulated from one another. cover 76 covers the rear of alternator 20, including rectifier 70. Electrical connectors (77) and 78) provide the required electrical connections to and from alternator 20. those connections are conventional, they described in detail here.

[0022] Referring now to Figures 2 and 3, a respective partial cutaway perspective view of a stator 54 is illustrated. Windings 58 with end turns 60 extending therefrom are positioned within slots 80 of stator core 56 in a conventional manner. In the illustrated embodiment 84 slots 80 were used. Preferably, full pitch windings are

used, i.e., opposite poles are 180° apart electrically. However, fractional pitches less than 180° may also be used.

Referring now to Figure 4, a schematic view of a first embodiment of a stator circuit 300 is coupled to a rectifier circuit 302. Stator circuit 300 has 2N+1 phases In the following examples, N=3 and therefore or windings. there are seven windings. The present invention applies equally to other circuits where N is an integer greater than Prior art systems typically use N=1 as in a three phase implementation. In this example, windings A, B, C, D, E, F and G are coupled schematically in a polygon. That is, each end of each of windings A-G is coupled to one end of another one of the windings. As illustrated, winding end A1, is coupled to winding end G_2 , winding end A_2 is coupled to winding end B_1 , winding end B_2 is coupled to winding end C_1 , winding end C_2 is coupled to winding end D_1 , winding end D_2 is coupled to winding end E_1 , winding end E_2 is coupled to winding end F_1 , and winding end F_2 is coupled to winding end G_1 .

[0024] Rectifier circuit 302 is a common type full wave rectifier circuit as it would be evident to those skilled in the art which has been expanded to accommodate the number of phases of the electrical machine. That is, preferably one pair of diodes is provided for each phase and therefore the number of diodes equals 2(2N+1) or 14 for the case where N=3. Those skilled in the art will, however, appreciate that a greater number of diodes may be used. Rectifier circuit 302, as illustrated has fourteen diodes 304-317. Each diode has an anode and a cathode. The cathodes of diodes 305, 307, 309, 311, 313, 315 and 317 are coupled together. The anodes of cathodes 304, 306, 308, 310, 312,

314 and 316 are coupled together. The cathode of diode 304 is coupled to the anode of diode 305. The cathode of diode 306 is coupled to the anode of diode 307. The cathode of diode 308 is coupled to the anode of diode 309. The cathode of diode 310 is coupled to the anode of diode 311. The cathode of diode 312 is coupled to the anode of diode 313. The cathode of diode 314 is coupled to the anode of diode 315. The cathode of diode 316 is coupled to the anode of diode 315. The nodes (N1-N7) between respective diode pairs 304 and 305, 306 and 307, 308 and 309, 310 and 311, 312 and 313, 314 and 315, and 316 and 317 receive the output from one of the winding intersections (e.g., A2:B1, B2:C1).

[0025] Referring now to Figure 5, a modified winding circuit 300' is illustrated. In this embodiment, the phases A-G are coupled in a star configuration to a common node N_8 . That is, winding ends A_1 '- G_1 ' are coupled to common node N_8 .

[0026] Rectifier circuit 302 is configured identically to that shown in Figure 4 except for the location from where they are coupled to stator circuit 300'. Each phase has one end coupled to stator circuit 302. That is, winding end A_2 ', B_2 '..., G_2 ' are coupled to nodes N_1 - N_7 . Optional diodes may be included at N8.

[0027] Referring now to Figure 6, a plot of current ripple versus electrical angle for a three-phase alternator of the prior art is illustrated. The current ripple has a magnitude T_1 that in the prior art corresponds to 0.13 amps.

[0028] Referring now to Figure 7, a seven-phase rectified output of an alternator such as that shown in Figure 4 is illustrated. In this example, the ripple current T_2 has a

peak current of 0.025 amps. As can be seen, this is a substantial reduction from a common three-phase alternator.

[0029] Referring now to Figure 8, the sound pressure levels of the new winding configuration shown in Figure 4 are illustrated with respect to an existing winding. As can be seen, the overall sound pressure levels are lower in a winding configuration according to the present invention.

[0030] While particular embodiments of the invention have been shown and described, numerous variations and alternate embodiments will occur to those skilled in the art. For examples, although a star and polygon configuration are illustrated, various combinations of the two meeting the 2N+1 criteria may also be formed. Accordingly, it is intended that the invention be limited only in terms of the appended claims.